



# Geometric Bounds on the Power of Adiabatic Thermal Machines

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## Introduction

Is there a fundamental bound on the power of microscopic thermal devices that operate close to Carnot efficiency?

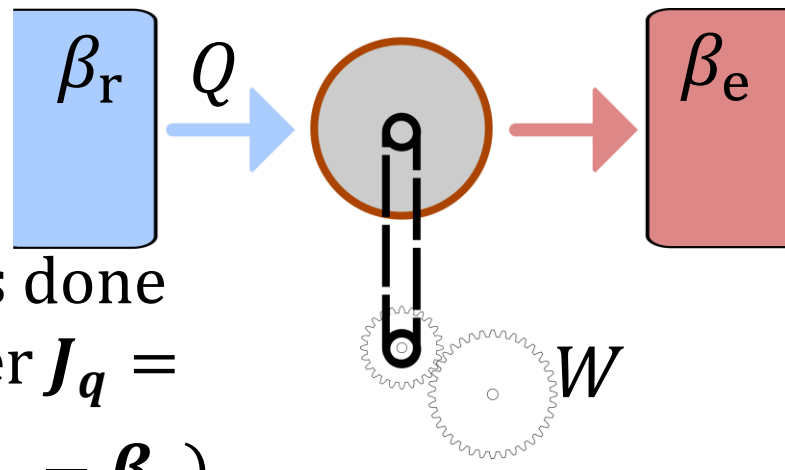
We show that the power of microscopic thermal machines, operating between two fixed temperatures, **decays quadratically** as Carnot efficiency is approached.

- This result presents a **geometric trade-off** between power and efficiency.
- The result is **universal** for devices with any kind of thermodynamically consistent dynamics, for both **refrigerators** and **heat engines**.

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## Microscopic Thermal Machines

We consider devices that operate between two heat baths  $\beta_r$  and  $\beta_e$ .



- **Refrigerator** ( $\beta_r > \beta_e$ ): work  $W \equiv J_w$ , is done during cycle period  $\tau$  with cooling power  $J_q = Q/\tau$  and efficiency  $\varepsilon = \frac{Q}{W} \leq \varepsilon_c \equiv \beta_e/(\beta_r - \beta_e)$
- **Heat Engines** ( $\beta_r < \beta_e$ ): work  $W \equiv J_w$ , is produced during cycle period  $\tau$ , uptake  $J_q = Q$  and efficiency  $\eta = \frac{W}{Q} \leq \eta_c = (\beta_r - \beta_e)/\beta_r$

## Adiabatic Response

The isothermal work,  $J_w^{\text{iso}}$ , and quasi-static heat current  $J_q^{\text{qs}}$  are defined.

$$J_w^{\text{iso}} = J_w \Big|_{A_q=0} = K_{ww} A_w \quad J_q^{\text{qs}} = J_q \Big|_{A_w=0} = K_{qq} A_q$$

Work input and heat flux,

$$J_w - J_w^{\text{iso}} = K_{wq} A_q \quad J_q - J_q^{\text{qs}} = K_{qw} A_w$$

- Affinities  $A_q = \beta_e - \beta_r$  and  $A_w = \beta_e/\tau$ .
- Onsager symmetry,  $K_{qw}|_{A_x \rightarrow 0} = -K_{wq}|_{A_x \rightarrow 0}$ , is assumed.

The efficiency, 
$$\frac{\varepsilon}{\varepsilon_c} = - \frac{K_{qw} + K_{qq} \left( \frac{A_q}{A_w} \right)}{K_{wq} + K_{ww} \left( \frac{A_w}{A_q} \right)}$$

As  $\tau \rightarrow \infty$ , Carnot efficiency can only be reached if the **quasi-static heat current**,  $K_{qq}$ , vanishes and if  $A_q \propto A_w^\alpha$  where  $0 < \alpha < 1$ .

Given  $A_q \propto A_w^\alpha$ , where  $0 < \alpha < 1$ , we expand the off diagonal coefficients in  $A_q$ ,

$$K_{qw} \rightarrow L_{qw} + L_{qw}^q A_q \quad K_{wq} \rightarrow L_{wq} + L_{wq}^q A_q$$

The work and heat current in **adiabatic response** (AR),

$$J_q = L_{qw} A_w + L_{qw}^q A_w A_q \quad J_w = L_{ww} A_w - L_{qw} A_q + L_{wq}^q A_q^2$$

## Thermodynamic Geometry

Thermodynamic quantities,

$$J_w = - \int_0^\tau dt f_t^\mu \dot{\lambda}_t^\mu, \quad J_q = \frac{1}{\tau} \int_0^\tau dt j_t$$

**Thermodynamic force**  $f_t^\mu$ , **instantaneous heat-current**  $j_t$ .

Set of control parameters  $\lambda_t$ .

$f_t^\mu$  and  $j_t$  are expanded,

- $f_t^\mu \simeq -\partial_\mu \mathcal{F}_{\lambda_t} - \beta_e \mathcal{R}_{\lambda_t}^{\mu\nu} \dot{\lambda}_t^\nu + \mathcal{R}_{\lambda_t}^{\mu q} A_q + \mathcal{R}_{\lambda_t}^{\mu qq} A_q^2$ ,
- $j_t \simeq \beta_e \mathcal{R}_{\lambda_t}^{q\mu} \dot{\lambda}_t^\mu + \beta_e \mathcal{R}_{\lambda_t}^{qq\mu} \dot{\lambda}_t^\mu A_q$

$\mathcal{R}_\lambda$  and  $\mathcal{F}_\lambda$  depend only on  $\lambda$  and  $\beta_e$ .

The AR coefficients have a **geometric interpretation**,

$$\begin{bmatrix} L_{wq} & L_{qw} \\ L_{wq}^q & L_{qw}^q \end{bmatrix} = \oint_\gamma \begin{bmatrix} \mathcal{A}_\lambda^{\mu q} & \mathcal{A}_\lambda^{q\mu} \\ \mathcal{A}_\lambda^{\mu qq} & \mathcal{A}_\lambda^{qq\mu} \end{bmatrix} d\lambda^\mu$$

**Thermodynamic potentials**  $\mathcal{A}_\lambda^{xyz}$  depend on coefficients  $\mathcal{R}_{\lambda_t}^{xyz}$ .  $\gamma$  is path taken in the space of control parameters.

## Approaching Carnot Efficiency

The efficiency under new scaling argument, 
$$\frac{\varepsilon}{\varepsilon_c} = 1 + \frac{L_{qw}^q + L_{wq}^q}{L_{qw}} A_q + \frac{L_{ww}}{L_{qw}} \frac{A_w}{A_q}$$

maximised with respect to  $A_q$ ,

$$\frac{\varepsilon}{\varepsilon_c} \leq 1 - \sqrt{A_w L_{qw} / Z} \quad \text{saturated if } A_q^* = -\sqrt{z A_w}$$

with  $Z = L_{qw}^3 / 4 (L_{qw}^q + L_{wq}^q) L_{ww}$  and  $z = L_{ww} / (L_{qw}^q + L_{wq}^q)$

## Main Result: Power-Efficiency trade-off

For refrigerators (heat engines), cooling power  $P_c$  (power  $P$ ),

$$P_c \leq Z (\varepsilon_c - \varepsilon)^2 / \varepsilon_c^2 \quad P \leq Z (\eta_c - \eta)^2 / \eta_c$$

- Power decays **quadratically** as Carnot approached.
- The **bound is geometric**. The **figure of merit**  $Z$  becomes **geometric**  $Z \rightarrow \mathcal{Z}$ , substituting the geometric AR coefficients.

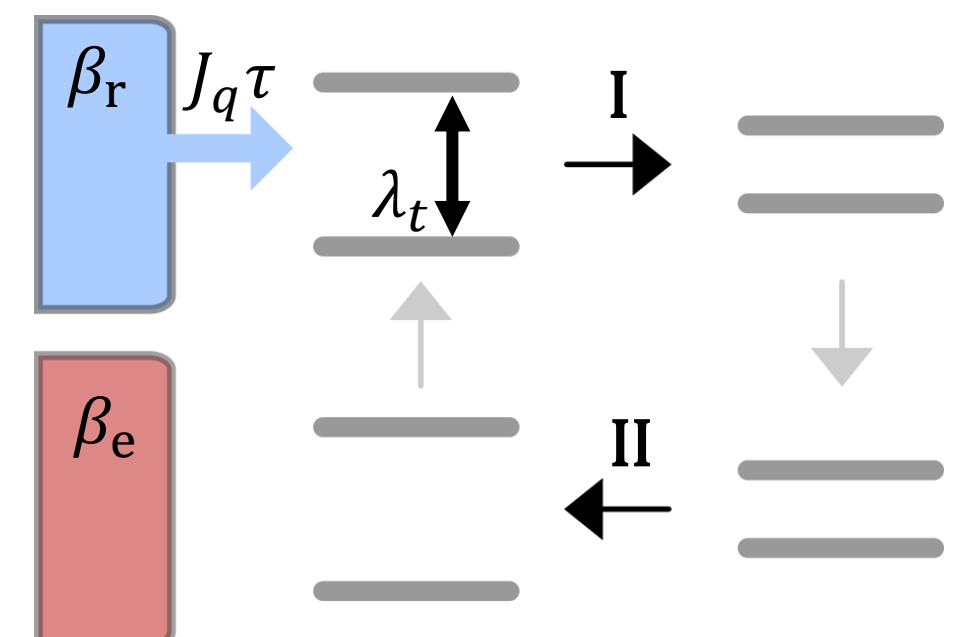
## Example: Two-Stroke Refrigerator

Single-qubit refrigerator: **Hamiltonian**,  $H_\lambda = \hbar \Omega \lambda_t \sigma_z / 2$  in a two-stroke cycle.

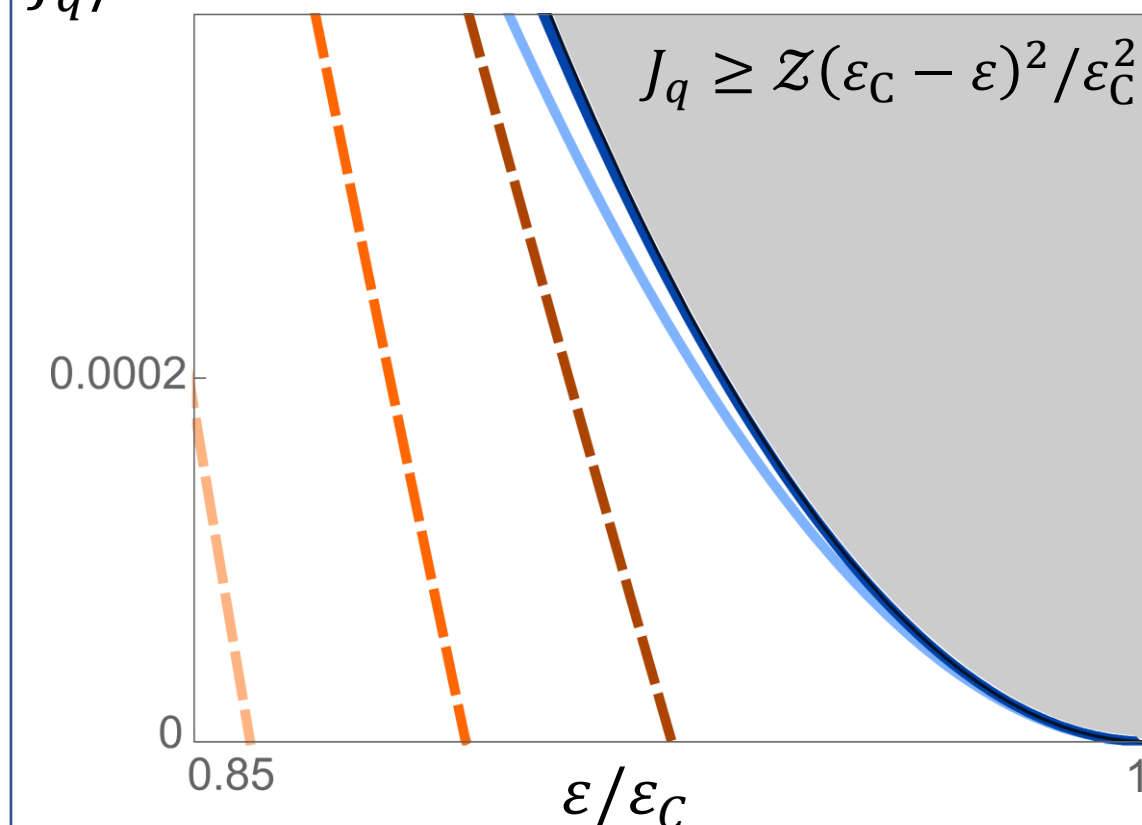
$\Gamma > 0$  sets relaxation timescale of system.

**Stroke I:** couple to  $\beta_r$ ,  $\lambda_0 \rightarrow \lambda_1$ .

**Stroke II:** couple to  $\beta_e$ ,  $\lambda_1 \rightarrow \lambda_\tau \equiv \lambda_0$ .



$J_q / \hbar \Omega \Gamma$

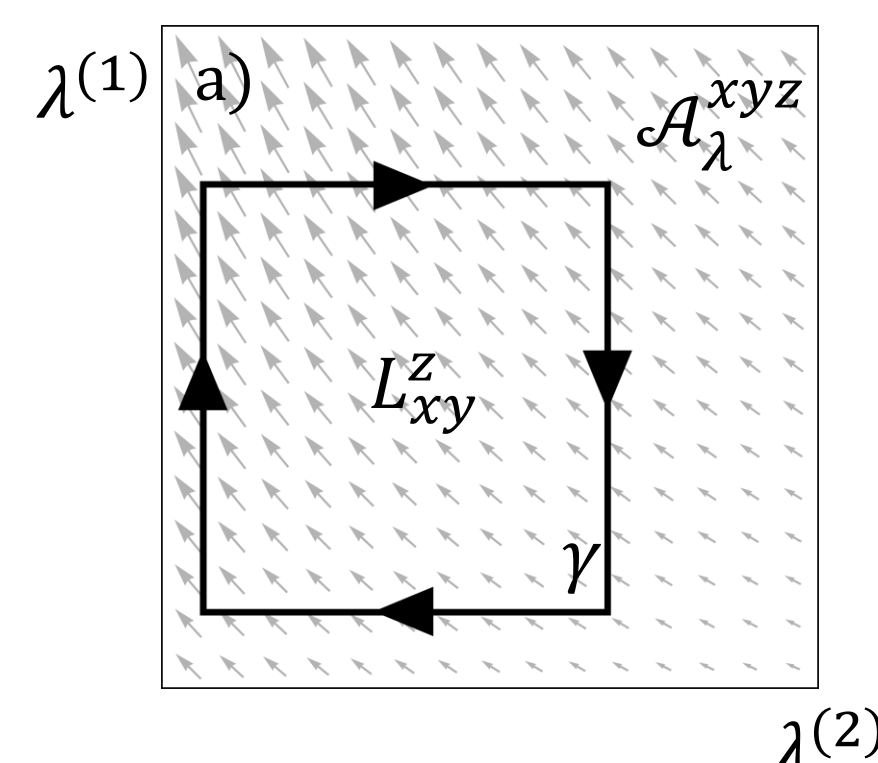


- Fixed  $A_q$  (dashed-lines)
- Unobtainable region (grey) is **geometrically bounded**.
- Bound saturated by **optimal scaling**  $A_q^*$  (light-blue) and **optimal driving** (dark-blue)

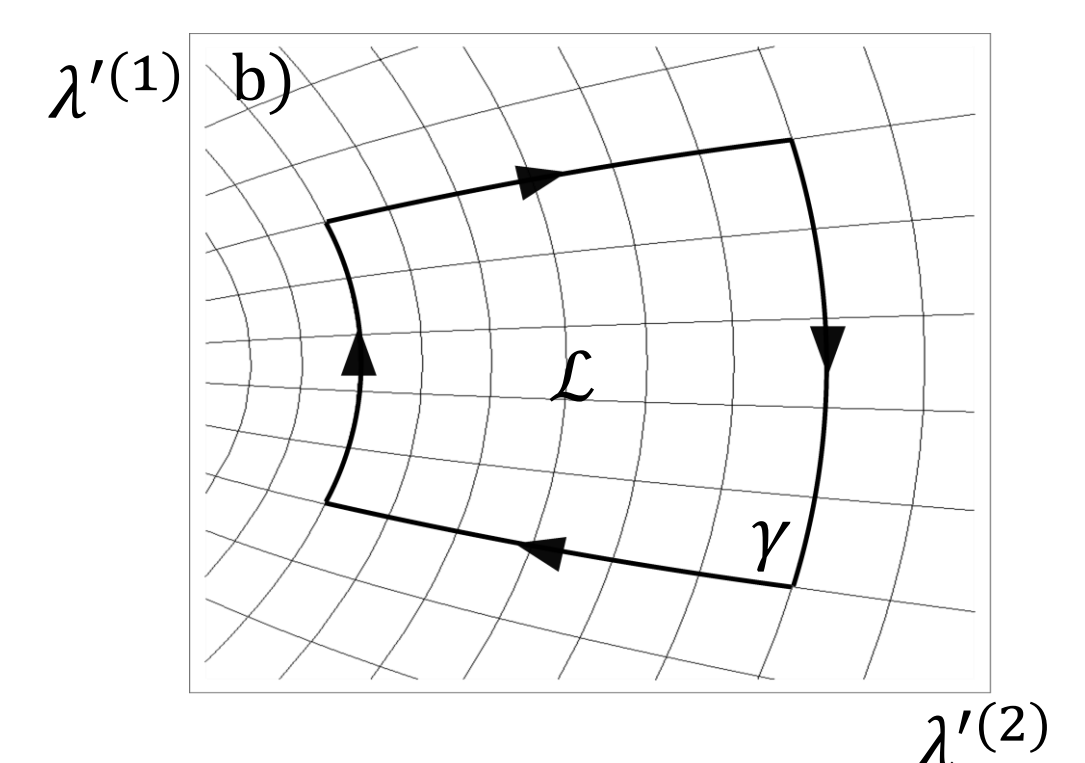
Coefficient  $L_{ww}$  has **geometric bound** corresponding to the **thermodynamic length**  $\mathcal{L}$  characterised by metric  $G_\lambda^{\mu\nu}$ .

$$L_{ww} \geq \mathcal{L}^2 \quad \text{where} \quad \mathcal{L} \leq \oint_\gamma \sqrt{G_\lambda^{\mu\nu} d\lambda^\mu d\lambda^\nu}$$

The bound is **saturated** by driving  $\lambda_t$  by the **optimal speed function**  $\phi_t$



a) Thermodynamic vector potential



b) Thermodynamic length in curvilinear coordinates  $\lambda \rightarrow \lambda'$